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核磁纸共鸣装置 日本業の名称

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明 編 書

- 1. 考案の名称 核磁気共鳴装置
- 2. 実用新案登録請求の範囲
- 3. 考案の詳細な説明 (産業上の利用分野)

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実開1-165010

この考案は人体の断層像により医療診断を行うための核磁気共鳴装置に関する。

〔従来の技術〕

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第2図は核磁気共鳴装置のマグネットの立面図、 第3図は同じく側面図で、マグネット1のすぐ近 くにベッド2とこのベッド2の上に患者3を敬せ で移動可能の移動台車22が設けられており、った ところで移動台車22をマグネット1の内部に ところで移動台車22をマグネット1の内部に ところで移動台車22をマグネット1の内部に ところで移動台車22をマグネット1の内部に ところで移動台車22をマグネット1の内部に ところで移動台車22をマグネット1の内部に ところで移動台車22をマグネット1の中の位置に 数けられている図示しない均一 磁場の中心位置に 患者が移動できるように穴11が数けられており、 患者はベッド2の上から穴11の中の磁場の中心 位置まで移動台車22によって移動される構成と なっている。

核磁気共鳴装置は、均一磁場の強度に比例した水素核の磁気共鳴周波数に一致した数MILLから数10MILLの高同波電磁波を高周波コイルで送信し、



共鳴した原子核が放出する同一周波数の共鳴信号を受信コイルで受信しこの受信信号を増幅しコンピュータ処理することにより患者の所定の断形の画像を得ることができる。

この点を第4図の核磁気共鳴装置の構成を示す 概念図を川いて更に詳しく述べると、マグネット 1の中に収納されている均一磁場コイルによって 生成された均一磁場空間内において、勾配磁場コ イル用電流発生器としての勾配磁場電源装置41A により生成した所定の彼形のパルス状態液を勾配 磁場コイルに流すことにより勾配磁場を生成して 所定の断層面を設定し、高周波電磁波送受信装置 43A に含まれる商周被電磁波の送信器により生成 した商閥波数電流を商周波コイルに流して商周波 催磁放を生起し、この高周波電磁放に共鳴した被 検体3の所定の断層面内の原子核が放出する共鳴 信号を両周波受信コイルを介して両周波電磁波送 受信装置43A に含まれる高周被受信装置で受信し、 この受信信号を中間周波数に周波数変換するなど の処理の後ディジタル信号に変換した上でコン



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ピュータイトに入力する。この入力信号を処理することによりコンピュータイトによる演算の結果として記憶装置上に画像データが構成され、この画像データがコンピュータイトに付属のCRT画面に適宜表示される。

このように核磁気共鳴装置においては種々の電子装置を連動させることにより、所定の断層画像を振像することになる。

第4図において、マグネット1とベッド2とはシールドルーム20内に収納されており、ベッド2の中には断層画像撮像の際の勾配磁場コイルの流送受信などの制御を一括して行うスキャンコントローラ42k と高間波送受信監役43kとが収納されており、マグネット1の中には関勾配磁場ではないの電力増幅器を主体とする勾配磁場である地域が収納されている構成とし、これらの直流を必要とする電子装置の電源としてよりので変数とする電子を介していたから、それでれるで変数は単独に交流を直流に変換する電流を直流に変換するで、

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電源回路を持っている.

コンピュータ 4 人の出力信号としての断層機像のための信号は信号ケーブル101 によってスキャンコントローラ42A が信号ケーブル 102 を介して勾配磁場電源41A に、図示しない信号ケーブルによって勾配磁場電源装置43A に、それぞれ所定の信号を出力し伝送する。

(考案が解決しようとする課題)

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前述のようにシールドルーム20の外部から各電子装置に対する交流電源や断層機像の保証をあった。 の信号をシールドルーム20内の各電子装置って、 はているが、これらの伝送ケーブルで、 なイズがシールドルーム20内に侵入するでで、 なイズがシールドルーム20内に侵入するになって、 のようなノイズの侵入を防止するな際にはそれで でから各電子装置に配線する際にはそれで れの電子装置に配線する際には111、112 を設けるとか、信号ケーブル101を含むでは を設けるとか、信号ケーブル101を含むでは を設けるとか、信号ケーブル101を含するは を設けるとか、信号ケーブル101を含するなけるない 対示しない高性能の高周波フィルターを設けるな

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どの対策を講ずるのであるが、絶縁トランス110、111、112 や高周波フィルターなどが高価であるとともに、核磁気共鳴を起こさせるための高周波電磁波の周波数が数M版から数十M版程度であるのでラジオ電波の周波数に近いために高性能の高間波フィルターを使用してもノイズの抑制が困難であるなどの問題がある。

この考案は安価でしかもラジオ電波などのノイスを行効に抑制した高性能の核磁気共鳴装置を提供することを目的とする。

〔課題を解決するための手段〕

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電力を生成する資流電源装置とを備え、前記電子 回路を前記マグネットまたは前記ペッドの中に収納し、前記資流電源装置を前記ペッドと前記すの記での記での記で子回路の道流電源入力端子と前記資流電源装置との所定の出力端子とを選続ケーブルで接続してなるものとする。

(作用)

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ことによって役入してくるノイズは安価な高周波フィルタで抑制することができる。

(実施例)

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以下この考案を実施例に基づいて説明する。第 1 図はこの考案の実施例の構成を示す概念図で、マグネット1 とベッド 2 とがシールトルーム 2 0 の中に設置され、勾配 磁場電源装置 4 1 がマグネット 1 内に、スキャンコントローラ 4 2 と新周波電磁波送受信装置 4 3 とがベッド 2 の中にそれぞれ収納されている構成については第 4 図の従来の構成と同一である。

勾配做場電源装置41、スキャンコントローラ42、高周被電磁波送受信装置43などはその中に交流を直流に変換して装置として必要な直流電力を得るための直流電源を持っていず直流ケーブル11、12、13を介してシールドルーム20の外部に設置してある総直流電源装置10によって必要とする直流電力を供給する構成としている。

総直流電源装置 1 0 は交流ケーブル 100 によって商用電力としての交流を受電し、これを整流し

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て複数の電子回路に必要とする電圧の複数の直流電力を生成する。このような交流を直流に整流して所望の電圧の直流電力を複数同時に得るような電源装置は交流電力を電源とした過常の電子装置には必ず使用されているものであり、その製作上の技術的問題はない。



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ある。第4図の絶縁トランスが不要になることは 勿論、前述のようにノイズカットが容易であるこ とから、高周波フィルターも価格の安いものを使 用することができるのでこの点でもコストダウン をすることができる。

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例と受光例とにそれぞれ設けられ発光部, 受光部とで成り立っているものである。

このようにこの考案を主としたノイズ対策を指すことによりマグネットやベッドの設置をを必要をある。 一ルドルーム20として低磁波シールドする数である。 を構成することができるので、核磁気共鳴を置の を構成することができるので、核磁気により ことができるので、核磁気により ないほどにより がないまとにより ないまかできる。

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装置43とは別の位置の受信コイルの極近伤に設置される構成とされるので、この前置増ี器の直接の直接の直接の直接の直接では、高間接の直接では、10から直接では、20回ではこれらを3を2の構成がとられる。この図ではこれらを3を3の3を1回路にも適用すべきものである。(考案の効果)

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4. 図面の簡単な説明

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20…シールドルーム、1…マグネット、

2 … ベッド、 3 … 被検体、

4. 4 人…コンピュータ、10 … 総直流電源装置、

- 1 3 -

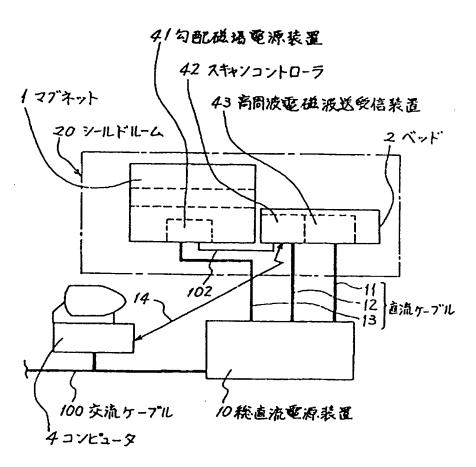
- 11,12,13…直流ケーブル、
- 14…光ケーブル、

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- 41,41 A … 勾配磁場電源装置、
- 4 2 . 4 2 A ... スキャンコントローラ、
- 43.43人…高周波電磁波送受信装置。

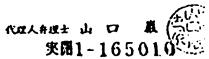
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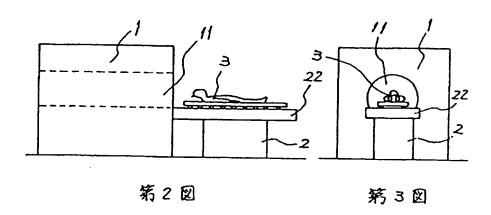


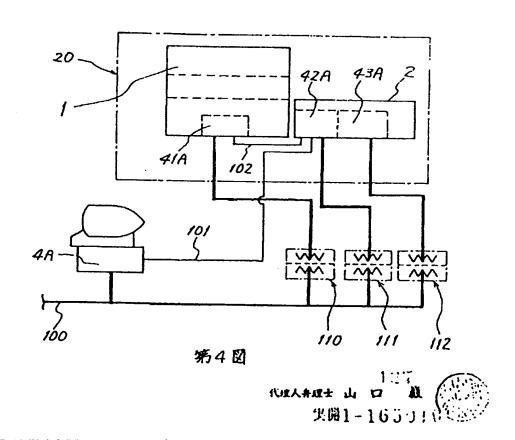


第1図

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(54) Title of the Device:

Nuclear Magnetic Resonance Apparatus

(21) Application No.:

63-60735

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May 9, 1988

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SPECIFICATION

1. Title of the Device:

Nuclear Magnetic Resonance Apparatus

2. Claims

1. A nuclear magnetic resonance apparatus characterized in that this is provided

with: a magnet comprising a case that houses a uniform field coil and a gradient field

coil; a bed on which a body to be examined lays; a scan controller for unified control of

tomography acquisition; an electronic circuit requiring DC power such as a gradient field

power source or a high-frequency transceiver controlled by this scan controller; and a

DC power supply device that receives AC current in the form of commercial power and

generates at least 1 DC power having a predetermined voltage; said electronic circuit

being housed in said magnet or said bed; said DC power supply device being located in

a position other than said bed and said magnet; and a DC power input terminal of said

electronic circuit being connected to a predetermined output terminal of said DC power

supply device by a DC cable.

3. Detailed Description of the Device

Field of Industrial Application

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This device relates to a nuclear magnetic resonance apparatus for medical

examination of the human body by means of tomography.

Prior Art

FIG. 2 is an elevated view of a magnet for a nuclear magnetic resonance

apparatus and FIG. 3 is a side view of the same; a bed 2 is provided immediately next

to this magnet 1, and on this bed 2 a mobile slide dolly 22 is provided on which a patient

3 lies; with the patient 3 reclining on the slide dolly 22, the slide dolly 22 is slid into the

magnet 1. An aperture 11 is provided so that the patient can be slid to a position

wherein the location on the patient at which the tomograph is to be acquired is aligned

with a central point in a magnetic field generated by a uniform field coil, a gradient field

coil, and the like, which is not shown in the drawing; the constitution is such that the

patient can be slid from the bed 2 into the aperture 11 to a central position in the

magnetic field by means of the slide dolly 22.

A nuclear magnetic resonance apparatus transmits high-frequency magnetic waves of

several MHz to several tens of MHz that match the magnetic resonance frequency of

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a hydrogen nucleus, which is proportional to the strength of the uniform field; a resonance signal of the same frequency emitted by the resonated atomic nuclei is received by a receiver coil; and this received signal is amplified and subjected to computer processing to produce an image of a specific section of the patient.

To describe this point in further detail, referring to the schematic view in FIG. 4, illustrating the structure of a nuclear magnetic resonance apparatus, within a uniform field space generated by a uniform field coil housed within the magnet 1, a pulsed current having a specific waveform generated by a gradient field power supply device 41A which serves as the current generator for the gradient field coil, is sent to the gradient field coil, whereby a gradient field is generated, and a specific sectional plane is set; the high-frequency current generated by the high-frequency electromagnetic wave transmitter, included in the high-frequency electromagnetic wave transceiver 43A, flows through the high-frequency coil to generate a high-frequency electromagnetic wave; the atomic nuclei in a specific sectional plane in the resonated test body 3 emit a resonant signal, which is received by the high-frequency receiver included in the high-frequency electromagnetic wave transceiver 43A by way of a high-frequency receiver coil; after such processing as frequency conversion to an intermediate frequency, this received signal is converted to a digital signal and

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then input to a computer 4A. The results of computations performed by the computer,

whereby this input signal is processed, constitute image data in a storage device; this

image data is conveniently displayed on a CRT associated with the computer 4A.

Thus, in a nuclear magnetic resonance apparatus, a specific tomograph is

acquired by linking the operations of various electronic devices.

In FIG. 4, the magnet 1 and the bed 2 are housed in a shield room 20; a scan

controller 42A, which has unified control over the gradient field coil current, the high-

frequency transmission and reception signals, and the like during tomography

acquisition, and the high-frequency transceiver 43A are housed in the bed 2; a gradient

field power source with a built-in power amplifier for the gradient field coil is housed in

the magnet 1; the power supply for these electronic devices which require DC power is

supplied from the exterior of the shield room 20 as AC power by way of isolating

transformers 110, 111, and 112, and each electronic device has a separate DC power

supply circuit that

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converts the AC to DC.

A tomography acquisition signal, which is an output signal from the computer 4A, is sent to the scan controller 42A by a signal cable 101; based on this signal, the scan controller 42A outputs and sends predetermined signals to the gradient field power supply 41A, via a signal cable 102, and to the gradient field power supply device [sic] 43A, via a cable not shown in the drawing.

Problems to Be Solved by the Device

As described above, the AC power for each of the electronic devices and the signals for tomography acquisition are sent to each of the devices within the shield room 20 from the exterior of the shield room 20, but since noise on these transmission cable gets into the shield room 20, in order to prevent noise from getting in, such countermeasures are taken as providing isolating transformers 110, 111 and 112 for each of these electronic devices when a power cable 100 is cabled to the various electronic devices, and providing high-performance high-frequency filters (not shown) at points where electromagnetism from the shield room 20 passes through the shielding, including at

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signal cable 101, there are problems in that, not only are isolating transformers 110, 111, and 112 and high-frequency filters expensive, but since the high-frequency electromagnetic waves which produce nuclear magnetic resonance have frequencies of several MHz to several tens of MHz, which are close to radio-wave frequencies, it is difficult to limit noise, even if high-performance high-frequency filters are used.

An object of this device is to provide a low-cost, high-performance nuclear magnetic resonance apparatus in which noise, such as radio waves, is effectively limited.

Means for Solving the Problems

In order to solve the aforementioned problems, according to this device: a magnet comprising a case that houses a uniform field coil and a gradient field coil; a bed on which a body to be examined lays; a scan controller for unified control of tomography acquisition; an electronic circuit requiring DC power, such as a gradient field power source or a high-frequency transceiver controlled by this scan controller; and a DC power supply device that receives AC current in the form of commercial power and generates at least 1 DC power having a predetermined voltage are provided; the

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electronic circuit being housed in the magnet or the bed; the DC power supply device being located in a position other than the bed and the magnet; and a DC power input terminal of the electronic circuit being connected to a predetermined output terminal of the DC power supply device by a DC cable.

Action

The constitution of this device is such that electrical circuits, such as the gradient field power source, the scan controller, and the high-frequency electromagnetic wave transceiver, which are operated directly for tomography acquisition, are housed in the magnet or the bed; the DC power supply for these electrical circuits is generated in a unified manner in a separately provided general DC power supply device; by virtue of a constitution wherein a predetermined DC power is supplied to each of the electronic devices by DC cables from this general DC power supply device, this general DC power supply device limits noise, such as radio waves, which gets into the nuclear magnetic resonance apparatus on an AC cable, which serves as the input to this general DC power supply device; and noise which gets in as a result of the DC cables acting as

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antennas that receive radio waves can be limited by an inexpensive high-frequency filter.

Embodiments

In the following, this device is described with reference to an embodiment. FIG. 1 is a schematic view illustrating the constitution of an embodiment of this device; the constitution is the same as the conventional constitution shown in FIG. 4, in that a magnet 1 and a bed 2 are provided in a shield room 20, and a scan controller 42 and a high-frequency electromagnetic wave transceiver 43 are each housed in the bed 2.

A gradient field power supply device 41, the scan controller 42, the high-frequency electromagnetic wave transceiver 43, and the like do not have within them DC power supply devices that convert AC current to DC current to produce the DC power required by the device; rather, the constitution is such that the required DC power is supplied by a general DC power supply device 10 provided at the exterior of the shield room 20, via DC cables 11, 12, and 13.

The general DC power supply device 10 receives AC current in the form of commercial power via an AC cable 100, rectifies it

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and generates a plurality of DC powers required by a plurality of electrical circuits. Power supply devices of this sort, which rectify AC current and simultaneously produce a plurality of DC powers having predetermined voltages are inevitably used in normal electrical terminals that use AC power as a power source, and there are no technical problems in terms of the manufacture thereof.

In the rectifier circuit which converts AC current to DC current, as a ripple component is superimposed on the rectified DC current, it is essential that a high-frequency filter be provided to limit this; furthermore, even if the DC cables act as antennas that capture radio waves which get into the electronic circuits as noise, the noise can easily be cut by inserting a high-frequency filter. Furthermore, in the prior art, the constitution was such that each electronic device had a rectifier circuit that converted AC current to DC current, thus unifying these in a general DC power supply device 10 does not involve an increase in cost; on the contrary, the device can be made more efficient by unification, and the constitution is such that, even in terms of DC power supplies alone, a cost reduction can be expected.

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It is a matter of course that the isolating transformers of FIG. 4 become unnecessary, and since, as described above, noise can easily be cut, inexpensive high-frequency filters can be used, which also allows for cost reduction.

FIG. 1, shows a further complete noise countermeasure wherein an optical transmission system is used with an optical cable 14 from a computer 4 to the scan controller 42 for command signals for tomography acquisition; as the signal sent by this optical transmission system with the optical cable 14 is a digital signal, it is particularly suited for optical transmission; furthermore, as high speed transmission is not necessary, this may be an optical transmission system that is fully realizable at current technology levels, and a common optical transmission system, using a quartz optical fiber as the optical cable, a light-emitting diode as the light-emitting element and a photodiode as the light-receiving element, is sufficient. Note that, as the data concerning the resonance signal, which is received from the scan controller 42, is sent to the computer 4, the representative optical transmission system shown by the optical cable 14 comprises a two-way optical fiber

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and transmission and reception units provided at a transmission end and a reception

end, respectively.

By virtue of implementing this device as a primary noise countermeasure, a

nuclear magnetic resonance apparatus can be constituted with such a greatly improved

S/N ratio that it is not necessary to electromagnetically shield the room in which the

magnet and bed are placed in a shield room 20, whereby electromagnetic shielding of

the room in which the nuclear magnetic resonance apparatus is placed can be omitted,

whereby cost reduction can be expected.

In FIG. 1, in addition to the [elements] described above, within the magnet 1

there is a shim coil for correcting the uniform field; DC current is supplied to this shim

coil. When this magnet is of the normal conducting type, the uniform field coil is a

normal conducting coil and therefore DC current is supplied to this normal conducting

coil. Since the power for both this shim coil and the uniform field coil are DC, they are

beyond the applicability of this device and a description and explanation thereof is

omitted. Furthermore, in terms of electronic devices, in addition to that illustrated in the

drawing, the constitution is such that, for example, a preamp which initially amplifies the

signal received by the reception coil

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is positioned in the vicinity of the pole of the receiving coil in a position separate from the high-frequency electromagnetic wave transceiver 43; thus the DC power for this preamp can also be supplied by way of a connection with the general DC power supply device 10 or may be supplied indirectly via the high-frequency electromagnetic wave transceiver 43. This has been omitted in the drawing but this device is also applicable to these electronic circuits which are not shown in FIG. 1.

Effects of the Device

As described above, this device is such that electronic devices such as a scan controller, a high-frequency electromagnetic wave transceiver, a gradient field power supply device and the like are provided in the magnet or the bed; the DC power which is the DC power supply for these electronic devices is produced from a commercial power AC power source by a separately provided general DC power supply device, and DC power of the required voltages is supplied to each of the electronic circuits, whereby noise that is transmitted by AC power supply cables and gets into [these devices] is effectively limited,

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while inexpensive high-frequency filters can be used to limit the noise that gets into these devices as a result of the reception of radio waves by DC cables that act as antennas; furthermore, there is no need for isolating transformers, which were necessary in cases where AC current [was converted] to DC current and supplied at each of the electronic circuits, whereby noise can easily be controlled and the S/N ratio can be improved, while allowing for a nuclear magnetic resonance apparatus having a decreased cost. Moreover, the constitution is such that, by combining this with noise countermeasures such as, for example, using optical transmission for signals such as command signals from the computer to the scan controller for tomography acquisition, it is possible to omit the electromagnetic shielding of the room in which the nuclear magnetic resonance apparatus is placed, and a cost reduction effect can be expected in this regard.

4. Brief Description of the Drawings

FIG. 1 is a structural schematic view illustrating an embodiment of this device; FIG. 2 is an elevated view of a nuclear magnetic resonance apparatus; FIG. 3 is a side view¹ of the same; and FIG. 4 is a schematic view showing the constitution of a conventional nuclear magnetic resonance apparatus.

20	shield room	1	magnet
2	bed	3	test body
4, 4A	computer	10	general DC power supply device
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¹ In the original Japanese, the two-character word "voltage" has been crossed out and replaced by the one-character word "view". To the right of the text, an annotation reads, "Two characters deleted. One character inserted."

11, 12, 13	DC cables
14	optical cable
41, 41A	gradient field power supply device
42, 42A	scan controller

43, 43A

high frequency electromagnetic wave transceiver

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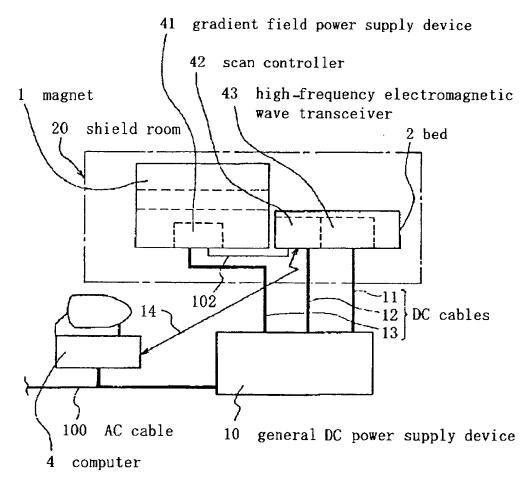


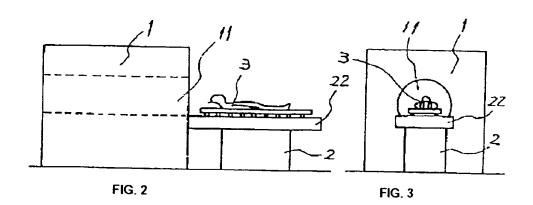
FIG. 1

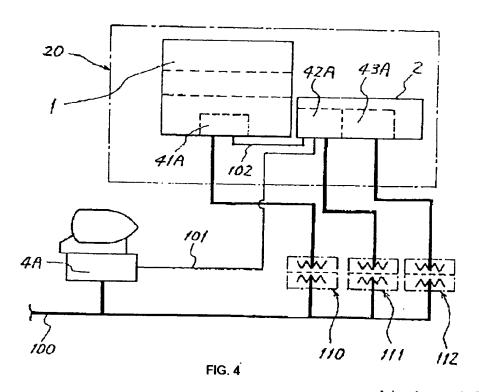
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